The Complete Cybenetics Test Protocol Including Energy Efficiency, Output Noise And Overall Performance Calculation of AC-DC Power Supplies

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Definitions

**AC Signal**
A time-varying signal whose polarity varies with a period of time T and whose average value is zero. [1]

**Ambient Temperature**
Temperature of the ambient air immediately surrounding the unit under test (UUT). [1]

**Apparent Power**
The product of RMS voltage and current (VA). It is also known as total power.

**DC Signal**
A signal of which the polarity and amplitude do not vary with time. [1]

**Efficiency**
The ratio, expressed as a percentage, of the total real output power to the real power input required to produce it, using the following equation:

\[ \eta = \frac{P_{out}}{P_{in}} \times 100 \]

The input power (Pin) includes the power that the cooling fans of the UUT require.

**PSU**
Power Supply Unit which converts one voltage to DC voltage output or outputs, depending on its type. In desktop PCs, PSUs with multiple DC voltage outputs (rails) are mainly used.

**IEEE Std 1515-2000**
The IEEE Std 1515 [1] is a basic specification language, providing parameter definitions, test conditions, and test methods. It does not attempt to standardize the specification itself. It provides the basis that allows everyone to speak the same language on a level playing field. This standard was withdrawn on 2019-11-07 [https://standards.ieee.org/standard/1515-2000.html], but we decided to use several of its definitions since they still apply.

**ATX Spec**
ATX (Advanced Technology eXtended) is a motherboard and power supply configuration specification developed by Intel in 1995 to improve on previous de facto standards like the AT design. [6]

**Output Voltage Ripple**
The maximum ac voltage present on a dc or low-frequency ac voltage stated in peak-to-peak voltage. The intent is to characterize the residual component associated with the switching action at the output switching frequency (or twice the output switching frequency).
**True Power Factor**
True power factor is the ratio of the active, or real, power ($P$) in Watts to the apparent power ($S$) in Volt-Amperes

$$PF = \frac{P}{S}$$

**Crest Factor**
The crest factor is the ratio of peak current to RMS current (or peak voltage to RMS voltage). For a pure sinusoidal wave shape the crest factor is 1.414, while for a pure constant DC load the crest factor is 1.0.

**Rail or DC Bus**
Any of the DC outputs of the PSU, which delivers power to the connected system. The standard rails for multi-rail PSUs are +12V, +5V, +3.3V, +5VSB with -12V being optional by the latest ATX specs.

**Rated AC Input Voltage Range**
The input voltage range (minimum/maximum) provided by the UUT manufacturer. It is shown on the power label of the UUT.

**Rated DC Output Voltage(s)**
Description

**Rated DC Output Power and Current**
The rated DC output power and current is the maximum load that a PSU can provide at a specified ambient temperature, on its rails. The DC output power and current output for each of the PSU’s rails is provided by the manufacturer and it is depicted on its power label and on the packaging. If there is any difference, we always take into account the power label on the PSU.

**RMS (Root Mean Square)**
The square root of the average of the square of the value of the function taken throughout the period. For instance, the RMS voltage value for a sine wave may be computed as:

$$V_{rms} = \sqrt{\frac{1}{T} \int_{0}^{T} V^2(t) dt}$$

Where $T$ is the period of the waveform,

$V(t)$ is the instantaneous voltage at time $t$

$V_{RMS}$ is the RMS voltage value.[1]
Steady State
The operating condition of a system wherein the observed variable has reached an equilibrium condition in response to an input or other stimulus in accordance with the definition of the system transfer function. In the case of a power supply, this may involve the system output being at some constant voltage or current value. [1]

Total Harmonic Distortion (THD)
The total harmonic distortion (THD or THDi) [7] is a measurement of the harmonic distortion present in a signal and is defined as the ratio of the sum of the powers of all harmonic components to the power of the fundamental frequency.

UUT
UUT is an acronym for "Unit Under Test," which refers to the PSU sample being tested.
Prologue

The purpose of this article is to clearly explain our methodologies and testing procedures, not only for efficiency and noise output results but for all significant performance aspects of a PSU, including ripple suppression, transient response, hold-up time, inrush current, etc.

This article will be a great source of information for all brands and manufacturers that want to check the compatibility of their products with our efficiency and noise standards (ETA and LAMBDA). Moreover, it will allow every laboratory with the proper equipment, to verify our results, as the ISO17025:2017 [8] dictates. To elaborate more on this, two labs with calibrated equipment that have the same capabilities and can offer similar levels of accuracy in results should come up with identical results, given that they follow the same methodology. Cybenetics aims to become a certification body, meaning that it will accept all results coming from ISO17025 certified labs that follow the provided methodology for obtaining the necessary data, from which the ETA and LAMBDA certifications derive.

So far the existing efficiency standards had many flaws which include among others the limited number of measurements (three to four), the very low ambient temperature at which the tests are conducted, lack of any standby rail measurements, and the absent of mention to the equipment used to perform measurements. Especially the latter is of immense importance since every proper testing report should include the equipment that was used to conduct all measurements.
Test Setup & Measurement Conditions

Unless otherwise specified, all measurements are conducted with the equipment and the conditions mentioned below.

Measuring Equipment

All measurements are performed using several fully-equipped Chroma 63600 stations. Each of them can deliver more than 4 kW of load and includes two 63601-5 and one 63600-2 mainframes. Each of the mainframes mentioned above hosts ten 63640-80-80 [400 W] electronic loads along with a two 63610-80-20 [100 W x2] modules. Finally, we have one Chroma 6314 station, which is currently held as a backup. It can deliver up to 2500 W of load and consists of two 6314A mainframes equipped with the following electronic loads: six 63123A [350 W each], one 63102A [100 W x2], and one 63101A [200 W].

The AC sources that we use are a Chroma 6530, capable of delivering up to 3 kW of power, a Chroma 61604, which is used in our inrush current test station, with 2 kW max capacity, and two Keysight AC6804B with 4 kW max power. All AC sources are connected to the mains network through powerful isolation transformers. Finally, we protect the AC sources, with CyberPower OLS3000E online UPS devices.
The rest of our equipment consists of three Picotech TC-08 thermocouple data loggers, two Fluke multimeters (models 289 and 175), a Keysight U1273AX multimeter, a Keithley 2015 THD 6.5 digit bench DMM, and three lab-grade N4L PPA1530 3-phase power analyzers, featuring 0.05% basic accuracy. For back-up purposes, we have a Yokogawa WT210 power analyzer and a GW Instek GPM-8212. Finally, we also have a highly accurate N4L PPA5530 3-phase power analyzer with 0.01% basic accuracy, used in our inrush current test station.

The noise measurements are conducted with Class 1 Brue & Kjaer sound analyzers (2270 G4 and 2250-L G), equipped with a type 4955-A low-noise and free-field microphones, which can measure down to 5 dB(A) (we also have type 4189 microphones that features a 16.6-140 dBA-weighted dynamic range). The sound analyzers are installed into a hemi-anechoic chamber, with a close to 6 dB(A) noise floor. A Brue & Kjaer Type 4231 is used before every noise measurement to calibrate the sound analyzers.

We can conduct Electromagnetic Compatibility (EMC) evaluations since our lab is equipped with a Rigol DSA815-TG Spectrum Analyzer (9kHz -1.5GHz), featuring the EMI option. We also use a Tekbox TBLC08 LISN to isolate the power mains from the device in this test (DUT). Our second Spectrum Analyzer is a Signal Hound BB60C. To identify the EMI source should the need arise, we have at our disposal a set of Tekbox EMC probes (TBPS01) and a TBWA2 wide-band amplifier.

Measuring Software – Faganas ATE

An essential part of our methodology is the control and monitoring software, which is connected to every piece of equipment that we use, even the hotbox. This application is developed for the past ten years, and it consists of thousands of lines of code.

Besides gathering all data, storing it, and allowing is to extract it in any possible form, which meets our requirements, one of its most vital functions is that it also allows us to average all readings that we get. Usually, we check each different load level for four to ten minutes, and
during this period, we don't just take any random reading, but we gather all of them, and we take the average readings as the final result. This is the only way to have highly accurate results because as the heat increases at the internals of the power supply and the resistance of the PSU's gauges changes, due to the temperature difference, it is natural to have voltage, load and efficiency differences. So the best way is to take all readings throughout a test into account and accept the average as the final result.

**Input Voltage & Max Watt Output**

Besides 115 V and 230 V, we also conduct testing at 100 V, to check on the PSU's performance with a lower voltage input. Since we push all PSUs hard, at high ambient temperatures close to 45°C, we avoid testing with an even lower voltage input (e.g., 90V), since a PSU failure can also damage the power analyzer, which is directly connected to it. By cranking up the heat inside the hotbox and by dialing higher loads than the nominal ones, we already apply huge stress to the DUT, especially with 100 V input, simulating some of the worst real-life scenarios.

We use the PSU's label to check on the max Watt output, and we also conduct a test with 110% load, of the PSU's max-rated-capacity with the operating temperature exceeding 45°C, in PSUs that claim to deliver continuous full load output at 50°C.

**Test Conditions**

The ambient during the efficiency and noise output testing is 30°C (+2°C). We also conduct tests at higher ambient temperatures, which are within the 35-45°C range (+2°C).
Efficiency Measurements Procedure

Contrary to existing methodologies, which only take three to four measurements, we choose to apply more than 1450 different load combinations in the DUT, with the whole procedure lasting about two and a half hours in total. The overall efficiency is the average of all measurements, which cover the PSU’s entire operational range. This way it is impossible for a manufacturer to tune its products to meet some specified load levels, since, in essence, we take under consideration the efficiency levels under a higher number of different load combinations, evenly spread throughout the full load range. Besides efficiency, we also take voltage, ripple, power factor, noise, and temperature measurements.

We try to have at least 20 different load levels at 5V and 3.3V. At the same time, we also set a suitable load step at +12V, which can deliver at least 1450, in total, load combinations at +12V, 5V, and 3.3V. Finally, we apply a steady load of 1A at 5VSB while we don’t deal at all with the -12V, which is not required anymore by the newest ATX spec.

A description of the algorithm used to derive the load levels on the rails mentioned above is provided below in code form. The output table contains all possible load combinations, given the +12V and 5V/3.3V Watt step output that we select. We also have an entry for the minimum applied load on the rails, because some older PSUs with a group-regulation scheme on the secondary side, cannot operate properly with zero load at +12V and full load on the minor rails (and vice versa). Finally, the load at 5VSB remains the same throughout these tests. We chose this for two reasons: this is a standby rail, so most likely, it won't be utilized while the PSU is in operation, and secondly, if we also employed this rail in the algorithm shown below, the corresponding testing would last much longer.
Max_12V_load = PSU_12V_max_power - V12_min_load  
Max_5V_load = (Minor_Rails_Max_Combined_Load /5) * 3  
Max_33V_load = (Minor_Rails_Max_Combined_Load /5) * 2  

Load_steps_12V := round(Max_12V_load / Watts_12V_step)  
Load_steps_5V := round(Max_5V_load / Watts_5V_33V_step)  
Load_steps_33V := round(Max_33V_load / Watts_5V_33V_step)  

for i := 0 to Load_steps_12V do  
    for k := 0 to Load_steps_5V do  
    {  
        l := k;  
        if l > Load_steps_33V then l := Load_steps_33V  

        total12V := V12_min_load + Watts_12V_step * i  
        total5V := V5_V33_min_load + Watts_5V_33V_step * k  
        total33V := V5_V33_min_load + Watts_5V_33V_step * l  

        if total12V + total5V + total33V <= PSU_Max_Power then  
        {  
            j = j + 1;  
            //Row Number  
            Load_combinations_table.Cells[0, j] = j  
            // 12V load  
            Load_combinations_table.Cells[1, j] = total12V  
            // 5V load  
            Load_combinations_table.Cells[2, j] = total5V  
            // 3.3V load  
            Load_combinations_table.Cells[3, j] = total33V  
        }  
    }  

The massive load of data that our methodology provides allows us to quickly modify our efficiency certification program, should this is required. Finally, we start our tests at close to 30 °C with the PSU inside a hotbox, which simulates a case environment. At the end of the test, the ambient temperature inside the box reaches up to 32-34 °C, so it is close to real-life conditions.

Vampire power (power consumption with no load on the 5VSB rail) is of high importance since all this amount of energy goes wasted, and most PC systems aren't kept in operation 24/7, meaning that for a significant part of the day the PSUs just consume energy without doing anything useful. We evaluate each PSU by following the EN 50564:2011 and IEC 62301 [2] measurement guidelines closely. In case the DUT doesn't meet our standards, it will be automatically downgraded to the next lower efficiency certification level. The whole procedure is easy to follow, in case you have an N4L power analyzer. With the PSU installed on one of our load testers and powered through one of our AC sources, we have it in standby mode and run the corresponding N4L application, which automatically collects all vampire power readings and provide us the full report after 15 minutes. During the process, if the TDH readings of the AC input go out of spec, the result is rendered as no valid, by the application.
Besides all the above, ETA will also take into account the overall efficiency of the 5VSB rail. We measure efficiency on this rail per 0.05 A steps up to its max current output, and the average of all measurements is the final efficiency result. We expect all PSUs to deliver over 70% overall efficiency output on this rail, with this threshold set even higher for units that fall into the top categories of the ETA program.
Output Noise Measurements Procedure

As we already mentioned in the efficiency measurements procedure, we apply at least 1450 different load combinations at +12V, 5V, and 3.3V on the DUT, while at the same time monitoring all vital data including the fan speed. With the fan speed range data in hand, we take noise measurements with as small intervals as possible, to have high accuracy, and we cover the entire range. For example, if the fan speed range is 400-2000 RPM, we take noise measurements per 50 RPM intervals.

The noise measurements are taken in a hemi-anechoic chamber with the DUT switched off and with its fan connected to an external power supply, which applies the voltage required to achieve the desired fan speeds. Moreover, the fan speed is continuously monitored by a tachometer. This way, we can eliminate third party noises, including the noise that the electronic loads make.

We make a table with the fan speed in RPM and the corresponding noise at that speed, an example of which can be found below. Afterward, our software looks into all data gathered during the load tests and assigns a decibel value to each fan speed value, with the help of the table above. The algorithm that performs this function is provided below.

Once we have a dBA value for each of the tests that we conducted, with multiple load combinations, we convert the dBA values to SPL to average them, and once this is done, we convert the final outcome to dBA again. This procedure allows us to have a single number describing the DUT’s overall noise output with at least 1450 different load combinations, and according to this number, we tax the DUT into one of the LAMBDA categories.

Besides the fan’s noise, we also check for electronic noise (coil whine), by applying a combination of loads to the DUT while it is installed in the hemi-anechoic chamber, using a passively-cooled load tester. If we find any electronic noise that exceeds 6-6.5 dB A, we have to take it into account if the lowest fan noise levels are within a 10 dBA range because it affects the noise measurements.

The easier way to do this is by conducting the corresponding fan noise measurements with a load applied to the DUT, to create the conditions that make it generate electronic noise. Based on our testing results so far, it is rare to find a power supply with higher than 6.5 dB A electronic noise at a one-meter distance, using a resistor-based load. In the majority of cases, coil whine noise is due to a combination of system parts. Finally, the applied scenario, which forces the PSU to emit electronic noise, also plays a notable role. Because a PSU might have electronic noise while it is switched on and without any load on its rails, but this is not a real-life scenario, so we don’t take it into account (but still we write down the results and notify the manufacturer about this issue). The same goes for operation with only the 3.3V rail having a load, or the 5V rail or both the minor rails (in PSUs with DC-DC converters though, for the generation of the minor rails, this means that the +12V rail is also in use since it powers the converters as mentioned above). On the contrary, we do take into account scenarios where the load is only applied at +12V, or at 5VSB (with the PSU in standby mode).
Background Noise Calculation

The background noise in our chamber can range from 5.5 dBA to 8 dBA, depending on the external conditions. To have the best possible conditions, we prefer to take our noise measurements during the night, where the ambient noise is lower compared to the day.

In no case, the background noise can exceed the sound of interest, and in practice, the output level of the DUT has to be at least 3 dBA higher than the background noise for the measurement to be accurate. Still, a correction has to be applied to get the correct result. The background noise correction by standard is defined as $K_1$ [9] [11], and it is the amount of which the measured source level is reduced to obtain background noise-corrected source level.

The procedure for measuring a DUT's noise output is the following:

- Measure the total noise level ($L_{DUT} + L_{BG}$) with the DUT in operation, paying extra attention to its lowest noise output mode.
- Measure the background noise level ($L_{BG}$) with the DUT switched off.
- Calculate the difference between the two aforementioned readings ($L_{DUT} - L_{BG}$). If it is less than 3 dBA, the background noise is too high to allow for an accurate measurement. If it is within a 3-10 dBA range, a correction has to be applied. There is no need for correction if the difference is greater than 10 dBA, but we still use it for up to 20 dBA differences.

The formula for calculating the noise source without the influence of the background noise is the following:

$$L_{DUT} = 10 \times \log\left(\frac{10^{L_{DUT}}}{10} - \frac{10^{L_{BG}}}{10}\right)$$

In a spreadsheet, the formula above can be given as $10^{\log(10^{LDUT}/10) - 10^{LBG}/10}$.
The chart above can be used to make background noise corrections to the source signal.

Output Noise Measurements Test Set Up

In the schemes below, you will find a scheme of our hemi-anechoic chamber with the exact placement of the MIC and the DUT. We strictly follow the corresponding ISO Standards [9][10].
Overall Performance Calculation

It is challenging to characterize the overall performance of a complex product like a power supply with a single number, since we conduct a vast amount of tests, and far too many factors have to be taken under consideration. Nonetheless, we have completed thousands of power supplies so far, and our database includes enormous amounts of data, which allowed us to find the best, up so far, possible algorithm for this job. We strive to continually improve through our methodology, so it is highly probable in the future to proceed with changes in this algorithm to make it even more accurate. Given that we already have all data in hand, it is easy to calculate again all overall performance scores of the PSUs listed in our database in every change that we might do in the performance algorithm.

Our overall performance algorithm takes into account all major performance factors:

- Load regulation
- Ripple suppression
- Transient Tests Response Deviation
- Voltage overshoots during Turn-On Transient tests
- Overall efficiency
- Efficiency with 2% load
- Overall 5VSB efficiency
- Overall Power Factor reading
- Hold-up time
- Power-ok signal
- Max Power
- PSU Timings
- PSU Protection Features

Load Regulation

In an ideal world, a PSU would maintain a constant voltage level regardless of load, but in real-life scenarios, there is always a voltage drop on each rail as the load increases. In our tests voltage regulation shows the difference between the initial voltage readings with 60W of load (and not with no load at all since many PSUs don’t work well with no load on their rails and some others feature no-load protection) and the voltage readings on all rails with a full load.

We calculate the voltage regulation rating of all ratings using the following equation:

\[ Eq_1 = 1.2 \times V.\text{Reg}_{+12V} + 0.6 \times (V.\text{Reg}_{+5V} + V.\text{Reg}_{+3.3V}) + 0.3 \times V.\text{Reg}_{5VSB} \]

In the formula above, you can see that 5V and 3.3V have a lower weighting factor and 5VSB the lowest. This is because the +12V rail is by far the most important in a system, and its stability is crucial. We use the same system in the other formulas below, too.
Ripple Suppression

Ripple represents the AC fluctuations (periodic) and noise (random) found in the DC rails of a PSU. We take the ripple readings of all rails from the 100% load test and combine them in the equation shown below.

\[ Eq_2 = 0.08 \times Ripple_{+12V} + 0.04 \times (Ripple_{+5V} + Ripple_{+3.3V}) + 0.02 \times Ripple_{5VSB} \]

Transient Response

How well a power supply reacts to sudden changes in load is a very good indication of the unit's power quality. We take the maximum deviation that each rail registered in all Transient Response tests we conduct, to calculate the performance.

We conduct a variety of transient tests:

- While the PSU is working at a 20 percent load state, a transient load is applied to the PSU for 20ms (15A at +12V, 6A at 5V and 3.3V, and 0.5 A at 5VSB).
- While working at 50 percent load, the PSU is hit by the same transient load.
- In the next tests, we use the same starting points, 20 and 50 percent load states again, however, we increase the load-changing repetition rate from 50 Hz (20ms) to 1 kHz (1ms). This way, we push even harder the PSU.
- In all tests, we measure the voltage drops that the sudden load change causes. The voltages should remain within the ATX specification's regulation limits.

\[ Eq_3 = 2 \times Max.\ Tran.\ Response_{+12V} + 0.2 \times (Max.\ Response_{+5V} + Max.\ Tran.\ Response_{+3.3V}) + 0.1 \times Max.\ Tran.\ Response_{5VSB} \]

Turn On Transient Voltage Overshoots

Performance calculation in these tests is rather simple since we use only the rough value of the registered spike, compared to the nominal value of +12V and 5VSB rails. At +12V, we use only the higher voltage overshoot and ignore the other one (if there is any, of course). To give an example: if the higher registered voltage overshoot at +12V is +12.5V, then the spike is 0.5V (12.5V – 12.0V), so we use this value in our equation.

\[ Eq_4 = 1.25 \times (Turn\_On\_Spike_{+12V} + Turn\_On\_Spike_{5VSB}) \]

Overall Efficiency

The average of all load combinations (>1450) that we applied to obtain the PSU's overall efficiency for the ETA certification.

\[ Eq_5 = 0.8 \times (100 - AVG\_Efficiency\_Score) \]
Efficiency at 2% of the max-rated-capacity load or 10W (for <500W PSUs)

According to the ATX spec [reference], the lowest DC load at Idle Mode is determined to be 10 Watts for mainstream computers. Computers with PSU larger than 500 Watts are also expected to have more components, and therefore the Idle Mode will be at a higher DC Load. The PSU above 500 Watts will use the Low Load Efficiency set at the 2% level.

\[ Eq_6 = 0.03 \times (100 - \text{Efficiency with 2\% or 10W load}) \]

Overall 5VSB Efficiency

The average of all load combinations that we applied to obtain the 5VSB rail's overall efficiency for the ETA certification.

\[ Eq_7 = 0.1 \times (100 - 5VSB\_AVG\_Efficiency\_Score) \]

Overall PF Score

The average of all load combinations (>1450) that we applied to obtain the PSU's overall PF score for the ETA certification.

\[ Eq_8 = 50 \times (1 - \text{Overall PF Score}) \]

Hold-up Time

Hold-up time represents the amount of time, usually measured in milliseconds, that a PSU can maintain output regulations as defined by the ATX specification without input power. Put simply, hold-up time is the amount of time that the system can continue to run without shutting down or rebooting during a power interruption. The ATX specification sets the minimum hold-up time to 17ms with the maximum continuous output load.

\[ Eq_9 = 0.15 \times (17 - \text{Hold up time}) \]

Power-ok Signal

According to the ATX spec, the PWR_OK is a "power good" signal. This signal should be asserted high, at 5V, by the power supply to indicate that the +12V, 5V, and 3.3V outputs are within the regulation thresholds and that sufficient mains energy is stored by the APFC converter to guarantee continuous power operation within specification for at least 17ms. Conversely, PWR_OK should be de-asserted to a low state, 0V, when any of the +12V, 5V, or 3.3V output voltages falls below its under-voltage threshold, or when mains power has been removed for a time sufficiently long such that power supply operation cannot be guaranteed. The AC loss to PWR_OK minimum hold-up time is set at 16ms, a lower period than the hold-up time, and ATX spec also sets a PWR_OK inactive to DC loss delay which should be more than 1ms. This means that in any case, the AC loss to PWR_OK hold-up should be lower than the overall hold-up time of the PSU and this ensures that in no case the power supply will continue sending a power good signal, while any of the +12V, 5V, and 3.3V rails is out of spec.
Given all the above, when the PWR_OK signal is higher than the hold-up time, we have a fake report by the PSU’s power ok signal, and our overall performance calculation algorithm deducts performance points. The PWR_OK signal’s hold-up time also has to be at least 1ms lower than the actual hold-up time, to provide enough time to the system to shut down before the voltage rails go out of spec.

If the PWR_OK signal is accurate, we use the following equation:

\[ Eq_{10} = 0.15 \times (PWR\_OK\_Hold\_up\_time - (Hold\_up\_time - 1)) \]

There are three scenarios here:

- The PWR_OK_Hold_up_time is exactly 1ms lower than the Hold_up_time, so the outcome is zero, meaning no difference to the overall score.
- The PWR_OK_Hold_up_time has larger than 1ms difference from the Hold_up_time, so the outcome is beneficiary for the overall score.
- The PWR_OK_Hold_up_time is higher than the (Hold_up_time – 1ms) period, so points are deducted from the overall score.

We should note that we don’t deduct points in this equation for lower than 16ms PWR_OK hold up time because in Eq6 we already deduct points for lower than 17ms hold-up time periods and in Eq7 the hold-up time is also involved.

Capacity

When you directly compare the load regulation, efficiency, or ripple readings of a 400W unit to those of a 1500W model, then the comparison is anything but fair.

For example, when looking at voltage regulation at 40W load, the regulation range for a 400W PSU is 360W (= 400W - 40W). However, when testing a 1500W model, it is much bigger: 1460W (= 1500W - 40W). With such a huge difference, it is natural that the smaller capacity unit will most likely register much better voltage regulation, or ripple. So we added a normalization that would set things right. This factor is directly derived from the rated power of each unit.

\[ Eq_{11} = 0.4 \times (\frac{Overall\_capacity}{100}) \]

PSU Timings

To meet the Alternative Sleep Mode, among others, the Power-on time (T1) needs to be lower than 150ms while the PWR_OK delay (T3) has to be within the 100-150ms range. Moreover, the T3 minimum time must not be faster than 100ms. For all units that meet the above requirements and also have higher than 16ms AC loss to PWR_OK hold-up time, and higher than 1ms PWR_OK inactive to DC loss delay, there is a bonus. We conduct the T1 and T3 measurements with two different load levels, 20%, and 100%. Each PSU needs to meet the requirements above in both cases.
If $T_1 < 150ms \& (T_3 > 100ms \& T_3 < 150ms) \& PWR\_OK \geq 16ms \& PWR\_OK\_Delay \geq 1ms$ then $PSU\_Timings\_Result = 1$

PSU Protections

Every power supply should be equipped with a proper protection scheme, which will allow it to operate safely even under harsh conditions, without breaking or causing any trouble to the system that it feeds with power.

The Over Current Protection (OCP) in all significant rails (+12V, 5V & 3.3V) along with the Over Power Protection (OPP) needs to be set within a proper range and not too high. When those protections are set high, the PSU might survive at normal temperatures, but there is a good chance that it will break at higher operating temperatures. Moreover, lots of stress is applied to its circuits, at high temperatures, so the OCP and OPP triggering points should be appropriately set. Surely a PSU has to be able to withstand high power spikes, usually deriving from GPUs and highly clocked CPUs, but at the same time, its protection features should ensure that its components are up to the task and not overloaded. According to our experience so far, the OCP for single +12V rail PSUs and OPP triggering points should be set within 130% of the respective nominal values. For PSUs with multiple +12V rails, we increase the allowed range to 135%.

The Over Temperature Protection (OTP) is among the most crucial protection features for each power supply. The majority of PSU failures are due to high operating temperatures, so there has to be a properly working OTP, which should be set according to the platform’s characteristics. Usually, in PSUs with a semi-passive operation, OTP is set a bit higher compared to PSUs, which lack passive operation.

The PWR_OK signal is of enormous importance when it comes to PSU protection features. Nonetheless, we already take into account the PWR_OK in Eq10, so there is no need to provide an extra bonus again.

Short Circuit Protection (SCP). If there is an output short circuit, which according to the ATX spec, is defined as any output impedance of less than 0.1 ohms, the PSU should shut down. The only exception here is the 5VSB rail, where the PSU is already in standby mode. Once the short circuit at 5VSB is removed, the PSU should come back in operation again without any problems.

The surge and inrush protections (SIP) are of high importance, and the PSU should be equipped with the appropriate parts to include those two protections. Usually, the surge protection is offered through a MOV (Metal Oxide Varistor). In contrast, the inrush protection involves an NTC thermistor which should be supported by a bypass relay, to provide enhanced protection levels.

We provide bonus points for each one of the following cases.

- 0.25 bonus: OCP at +12V, 5V, and 3.3V within 130% of the respective max-rated-capacity of the rail either from the factory or through software (if the PSU allows for software control). For PSUs with multiple +12V rails, we allow for up to 135% OCP triggering points.
• 0.25 bonus: OPP within 130% either from the factory or through software.
• 0.25 bonus: OTP that is shutting down the PSU at <190 degrees Celsius on the secondary heat sink or the secondary side in general
• 0.25 bonus: SCP on all rails. The PSU should work properly after prolonged and repetitive SCP evaluation tests.
• 0.25 bonus: The PSU should be equipped with a MOV or a TVS diode (or a combination of both)
• 0.25 bonus: The PSU should be equipped with an NTC thermistor and a bypass relay

If a PSU fails during the protection features evaluation testing within the conditions described above (e.g., with a within 130% of its max-rated-capacity load or with less than 190 degrees Celsius heat on the secondary side, there will be no point awards for the respective category that led to the PSU's failure. On the other hand, a PSU that meets all the above requirements is awarded two and a half (2.5) bonus points.

**Overall Performance Rating Calculation**

Now that we have calculated all the above factors, it's time to combine them to calculate the final performance rating (12). We take 100 as the perfect score and start subtracting results (1-10) and finally take into account the capacity (11) along with the PSU Timing and Protection Features bonus points.

\[
E_{12} = 100 - \sum_{k=1}^{10} E_{eq_k} + E_{eq_{11}} + PSU \text{ Timing Bonus} + PSU \text{ Protection Bonus}
\]

The result of (12) is the unit's overall Performance Rating.
Overall Performance Rating Calculation Examples

**Example A**

For this example we will use the **Wentai Aidan T1616** with 115V input:

\[
E_{q1} = 1.2 \times 0.3 + 0.6 \times (1.48 + 2.4) + 0.3 \times 2.44 = 0.36 + 2.328 + 0.732 \\
= 3.42 \text{ (Load Regulation)}
\]

\[
E_{q2} = 0.08 \times 27.46 + 0.04 \times (10.28 + 12.88) + 0.02 \times 14.44 = 2.1986 + 0.9264 + 0.2888 \\
= 3.4138 \text{ (Ripple Supression)}
\]

\[
E_{q3} = 2 \times 0.49 + 0.2 \times (1.63 + 3.05) + 0.1 \times 1.54 = 0.98 + 0.936 + 0.154 \\
= 2.07 \text{ (Transient Response)}
\]

\[
E_{q4} = 1.25 \times (0.12 + 0) = 0.15 \text{ (Turn - on Transient Response)}
\]

\[
E_{q5} = 0.8 \times (100 - 92.713) = 5.8296 \text{ (Overall efficiency)}
\]

\[
E_{q6} = 0.03 \times (100 - 77.432) = 0.67704 \text{ (Efficiency with 2% load)}
\]

\[
E_{q7} = 0.1 \times (100 - 82.381) = 1.7619 \text{ (Overall 5VSB efficiency)}
\]

\[
E_{q8} = 50 \times (1 - 0.99) = 0.5 \text{ (Overall PF score)}
\]

\[
E_{q9} = 0.15 \times (17 - 26.2) = -1.38 \text{ (Hold - up time)}
\]

\[
E_{q10} = 0.15 \times (25.2 - (26.2 - 1)) = 0 \text{ (Power Ok signal hold - up time)}
\]

\[
E_{q11} = 0.4 \times \left(\frac{1616}{100}\right) = 6.464 \text{ (Capacity)}
\]

**PSU Timings Bonus:** 0 (since T1 > 150ms in the 20% load test and T3>150ms in both tests)

**PSU Protections Bonus:** **OCP:** 0 (since 12V4 exceeds 135%), **OPP:** 0.25 (within 130%), **OTP:** 0.25 (<190°C), **SCP:** 0.25, **MOV:** 0.25, **NTC Thermistor & Relay:** 0.25

**Performance Rating** = 100 - 3.42 - 3.4138 - 2.07 - 0.15 - 5.8296 - 0.67704 - 1.7619 - 0.5 + 1.38 + 0+ 6.464 + 0 + 1.25 = 91.27166
Example B

For this example we will use the Corsair AX1600i with 115V input:

\[ Eq_1 = 1.2 \times 0.24 + 0.6 \times (0.9 + 0.3) + 0.3 \times 1.32 = 0.288 + 0.72 + 0.396 = 1.404 \quad (\text{Load Regulation}) \]

\[ Eq_2 = 0.08 \times 10.33 + 0.04 \times (6.24 + 14.98) + 0.02 \times 6.62 = 0.8264 + 0.8488 + 0.1324 = 1.8076 \quad (\text{Ripple Supression}) \]

\[ Eq_3 = 2 \times 0.64 + 0.2 \times (1.4 + 2.87) + 0.1 \times 1.28 = 1.28 + 0.854 + 0.128 = 2.262 \quad (\text{Transient Response}) \]

\[ Eq_4 = 1.25 \times (0 + 0.024) = 0.03 \quad (\text{Turn – on Transient Response}) \]

\[ Eq_5 = 0.8 \times (100 – 92.221) = 6.2232 \quad (\text{Overall efficiency}) \]

\[ Eq_6 = 0.03 \times (100 – 78.233) = 0.65301 \quad (\text{Efficiency with 2% load}) \]

\[ Eq_7 = 0.1 \times (100 – 81.807) = 1.8193 \quad (\text{Overall 5VSB efficiency}) \]

\[ Eq_8 = 50 \times (1 – 0.992) = 0.4 \quad (\text{Overall PF score}) \]

\[ Eq_9 = 0.15 \times (17 – 26.7) = -1.455 \quad (\text{Hold – up time}) \]

\[ Eq_{10} = 0.15 \times (24.5 – (26.7 – 2.2)) = 0 \quad (\text{Power Ok signal hold – up time}) \]

\[ Eq_{11} = 0.4 \times \left(\frac{1600}{100}\right) = 6.4 \quad (\text{Capacity}) \]

PSU Timings Bonus: 0 (since T1 > 150ms in the 20% load test and T3>150ms in both tests)

PSU Protections Bonus: OCP: 0.25 (since 12V not exceeds 135%), OPP: 0.25 (within 130%), OTP: 0.25 (<190°C), SCP: 0.25, MOV: 0.25, NTC Thermistor & Relay: 0.25

Performance Rating = 100 – 1.404 – 1.8076 – 2.262– 0.03 – 6.2232 – 0.65301 – 1.8193 – 0.4 + 1.455 + 0+ 6.4 + 0 + 1.5 = 94.75589
EFFICIENCY AND NOISE LEVEL CERTIFICATIONS

Test Report Example

Cybernetics

Anex

Lab ID: CR16001631
Receipt Date: Apr 1, 2020
Test Date: Apr 1, 2020

DUT INFORMATION

- Brand: Corsair
- Manufacturer (OSM): Xantec
- Series: AX
- Model Number: AX1600i (Sample #3)
- Serial Number: 17429560000000400227
- DUT Notes: Balanced Profile

DUT SPECIFICATIONS

- Rated Voltage (Vrms): 100-240
- Rated Current (Amps): 18.4
- Rated Frequency (Hz): 50/60
- Rated Power (W): 1600
- Type: ATX12V
- Cooling: 140mm FDB Dynamic Bearing Fan (4514PP)
- Semi-Active Operation: Yes (Selectable)
- Cable Design: Fully Modular

POWER SPECIFICATIONS

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CABLES AND CONNECTORS

- Modular Cables:
  - ATX connector 20-pin (600mm)
  - 4+4 pin EPS12V (600mm)
  - 6+2 pin PCIe (600mm)
  - 6+2 pin PCIe (600mm+100mm)
  - SATA (6Gbps x2+120mm+120mm+120mm)
  - SATA (6Gbps+120mm)
  - 4-pin Molex (450mm+100mm+100mm)
  - FDD Adapter (x 100mm)
  - USB Mini to Motherboard Header Cable (x 800mm)
  - AC Power Card (x 400mm) - C10 coupler

All data and graphics included in this report can be used by any individual under the following conditions:

- It should be mentioned that the test results are provided by Cybernetics.
- The link to the original test report document should be provided in any case.

Cybernetics offers the ETA and Lambda voluntary certification programs, through which the efficient and silent power supplies are promoted.

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4004 NESA GEFORA, LIMASSOL, CYPRUS
Epilogue

The purpose of this article was to explain the methodology that we follow for our efficiency and noise measurements, from which the ETA and LAMBDA certifications derive. We do want to share the knowledge that we have acquired after numerous PSU evaluations and help other laboratories with the proper equipment and the corresponding ISO certification (17025), which proves that all procedures will be followed in detail, test against our standards.

Besides providing a full insight into our efficiency and noise methodology, we decided to take one more (big) step and update and present our overall performance algorithm. Through this algorithm, someone can make highly detailed comparisons between any number supplies, taking into account all crucial factors, including protection features, besides pure performance. The development of this algorithm, which we will continue to update based on new data and experience that we gather through time, is a hard task. We plan to use this algorithm in our beta evaluations, and we will also share it with two major IT sites (Tom's Hardware and TechPowerUp), to help them provide more accurate comparison results.
References


[10] ISO 11201:2010 (E) - Acoustics - Noise emitted by machinery and equipment – Determination of emission sound pressure levels at a work station and at other specified positions in an essentially free field over a reflecting plane with negligible environmental corrections